

# SYNERGISTIC EFFECT OF CO-SUPPORTIVE OPEFB-MWCNT CONDUCTIVE NETWORK FOR HIGH-PERFORMANCE EMI SHIELDING APPLICATION

\*<sup>1</sup>Ismail Ibrahim Lakin, <sup>1</sup>Asiya Hassan, <sup>2</sup>Rabi'u Abubakar Tafida, <sup>3</sup>Ibrahim Abubakar Alhaji

<sup>1</sup>Department of Physics, Faculty of Physical Sciences, Kaduna State University, Kaduna, Nigeria

<sup>2</sup>Department of Physics, Nigerian Defence Academy, Afaka, PMB 2109, Kaduna, Nigeria

<sup>3</sup>Department of Physics, Faculty of Science, Federal University of Kashere, P.M.B. 0182, Gombe, Gombe State, Nigeria

\*Corresponding Author Email Address : [ismaillakin59@gmail.com](mailto:ismaillakin59@gmail.com)

## ABSTRACT

The crystallinity, microstructure, complex permittivity, and electromagnetic interference (EMI) shielding effectiveness (SE) of polymeric material filled with nanofiller were investigated. The nanofiller was multiwalled carbon nanotubes (MWCNTs). In addition, the EMI SE mechanism and dielectric properties in the X-band frequency were studied. The nanocomposites were fabricated by the melt-blending method. The effect of 5-13 wt.% MWCNTs filler on the dielectric of OPEFB/PLA/MWCNTs composites was studied. It was found that 13 wt.% MWCNTs exhibited the highest EMI SE value compared to 5, 7, 9, and 11 wt.% MWCNTs.

## INTRODUCTION

Currently, Electromagnetic (EM) radiation has proved to be the fourth most crucial source of public pollution, besides air, water, and noise pollution. It affects the typical behavior of systems or devices as well as is harmful to all living beings. Hence, there is an increasing demand for the development of suitable materials to attenuate the effects of the EM radiation (Cheng et al., 2021; Shahzad et al., 2016; Abbasi et al., 2019; Wang et al., 2020; Ma et al., 2020; Liang et al., 2021).

Microwave absorbers have dielectric and magnetic losses according to the type of filler used, and in general, absorption performance is dependent not only on their dielectric (permittivity) and magnetic (permeability) properties but also on the thickness and frequency. The magnetic absorbers are generally characterized by higher weight, thinner matching thickness, poor absorbing characteristics at high frequencies, and wider absorbing bandwidths in comparison with dielectric ones (Al-Saleh et al., 2013; Thomassin et al., 2013; Qin & Brosseau, 2012).

In developing absorbing composites, ferrites are commonly used. However, like any other metals, ferrites are heavy, corrosive, expensive, and non-biodegradable. Therefore, the use of metals such as ferrites for EMI shielding could lead to galvanic corrosion, which in turn increases the nonlinearity behavior and decreases its shielding effectiveness (Shifa et al., 2020; Soares et al., 2021). The conductive polymer has been used as an EMI shielding material for the merits of easy processing, chemical corrosion resistance, and light weight (Srivastava & Kumar, 2012; Tian et al., 2023).

Recently, researchers have paid close attention to polymeric nanocomposites for their enhanced electron mobility and electromagnetic absorption characteristics. EMI shielding effectiveness (SE) of the polymeric nanocomposites usually depends on the nanofiller type. Carbon nanotubes (CNTs) are one-dimensional carbon-based nanofillers with an aspect ratio,

outstanding mechanical strength, and strong dielectric polarization properties that are widely employed in the field of EM shielding materials (De Volder et al., 2013; Ma et al., 2023; Wang et al., 2021; Lai et al., 2022). Among them, multi-walled carbon nanotubes (MWCNTs) have received extensive attention from researchers due to their inexpensive cost and superior processing features (Liu et al., 2021; Zhou et al., 2022; Novoselov et al., 2013). Natural fibers have been utilized as reinforcing materials in combination with polymeric materials. Biofibers are used in polymeric composites due to their easy separation, low cost, low density, toughness, enhanced energy recovery, and significant biodegradability (Saba et al., 2014). The development of natural fiber composites has attracted research interest from various fields in the last few years because the fibers can replace conventional reinforcement materials in terms of weight reduction (Kumar & Sekaran, 2014). Oil palm empty fruit bunch (OPEFB) reinforced materials could reduce costs, enhance dielectric properties, thermal stability, and increase stiffness (Ahmad et al., 2017). Polylactic acid (PLA) is a thermoplastic polyester flexible and obtained mostly from materials that are renewable annually. PLA has high strength, elasticity modulus, stiffness, fragility, and is a biodegradable matrix (Abdalhadi et al., 2018). Reinforcing thermoplastics with cellulosic fibers, however, considerably increases rigidity and strength while drastically reducing composite toughness (Dike, 2022). PLA loaded with carbon nanotubes, graphite nanoplatelets, and other nanocarbons is among the best candidates for the production of structures with various sophisticated geometries through additive manufacturing (Yan et al., 2016).

In this study, the dielectric properties and absorption characteristics of OPEFB/PLA/MWCNTs nanocomposites were discussed. A total of 5-13 wt.% of MWCNTs filler loads were added into the OPEFB/PLA matrix to fabricate composites via the melt-blend technique and characterized at 8-12 GHz range. The electric field distributions due to material absorption were also examined. The main aim of this study was to examine the impact of various MWCNT loadings on dielectric permittivity and absorption characteristics of the OPEFB/PLA/MWCNTs nanocomposite materials.

## EXPERIMENTAL

### OPEFB/PLA/ MWCNTs composite preparation

The OPEFB FIBER was obtained from Bola oil mills, Oredo, Nigeria. To remove the wax layer of fibers, the OPEFB fibers were soaked in distilled water for 24 h. The fibers were rinsed with acetone and dried in an oven at 80 °C for 6 h to reduce the

moisture. The dried fibers were crushed into powder using a crusher machine (Mailand, Hunan, China), which was then sifted 100  $\mu\text{m}$  by laboratory test sieve (Endecotts, London, England). PLA was bought under the trade name polylactide resin 3052D from NatureWorks LLC (Minnetonka, MN, USA). Short MWCNTs were purchased from US Research Nanomaterials, Inc. (3302 Twig Leaf LN, Houston, TX 77084, USA) with > 95% purity. A total of 50 g of each sample was prepared for blending. The OPEFB/PLA/MWCNTs composites were fabricated by mixing 6%, 10%, 14%, 18%, and 22% mass percentages of MWCNTs with OPEFB fiber and PLA at a fixed ratio of 3:7. The PLA was melted in a Brabender Internal Mixer for 2 min at 150 °C with 50 rpm of rotor speed. Then the OPEFB fiber and MWCNTs powders were added and continued blending for another 12 min. The compression of the composites was done using the hydraulic hot press at 120 °C molding temperature, 150 kg/cm<sup>2</sup> pressure, for 10 min, (as illustrated in Figure 1) then cooled at 30 °C for 10 min.



**Figure 1.** Fabrication of OPEFB/PLA/MWCNTs composites

### Characterizations

#### X-Ray Diffraction (XRD)

The crystallinity of PLA, OPEFB, and OPEFB?PLA/MWCNTs composites were analyzed using a Shimadzu XRD 600 diffractometer (Tokyo, Japan) with a nickel-filtered Cu-  $\text{K}\alpha$  ( $\lambda = 0.1542 \text{ nm}$ ) beam at a voltage of 30 kV and a current of 30 mA. The composites were examined with a scanning rate of 2° /min at 25 °C within a 2 theta range of 10° to 80°.

#### Field Emission Scanning Electron Microscopy (FE-SEM)

The morphology of the samples (PLA, OPEFB, and OPEFB/PLA/MWCNTs) were examined using FE-SEM (Nova NanoSEM 230, FEI Holland) at a fixed voltage of 10 kV. The samples were coated with gold using a Bio-Rad (Hercules, CA, USA) coating system and then dried in an oven for 30 min to provide better conductivity.

#### Dielectric Properties Measurement

The measurements for the complex permittivity of the composites were carried out using the open-ended coaxial (OEC) probe. The probe was connected to an Agilent Network Analyser (VNA, Agilent Technologies, CA, USA) via a high-precision coaxial test cable

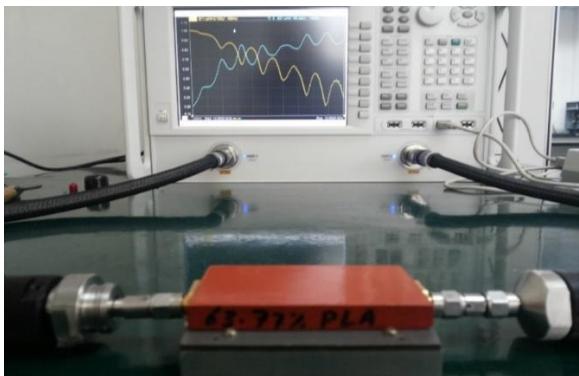
(Mensah *et al.*, 2019). A standard one-port, short-air-water calibration was performed, and a reference standard material (Polytetrafluoroethylene) was characterized to validate the accuracy of the calibration. As illustrated in Figure 2, the OEC probe was then firmly positioned on the flat surface of the samples to determine complex permittivity using the software installed on the VNA. All the measurements were performed at a frequency range of 8-12 GHz.



**Figure 2.** Complex Permittivity measurement using open-ended coaxial probe.

#### Measurement of Scattering Parameters (S-parameters)

The S-parameters were measured using a microstrip line (6 × 5) cm<sup>2</sup> in dimension connected to an HP8720B VNA through the two-port configuration as shown in Figure 3. The measurements were performed at a frequency range from 8 to 12 GHz. The composites to be measured were covered with a copper foil in order to avoid dispersion of radiation excited through the composite. Firm contact was ensured between the composite base and the microstrip line to avoid air gap during the measurement (Giita *et al.*, 2012).



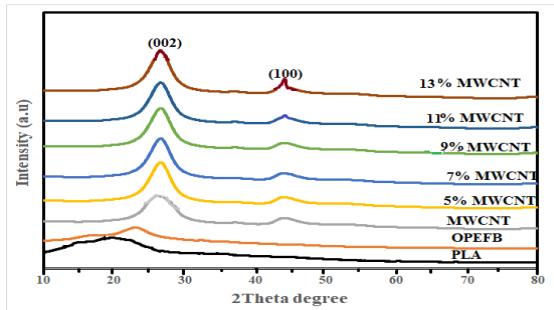
**Figure 3.** Set-up of S-parameters measurement using the microstrip sensor.

### RESULTS AND DISCUSSION

#### X-Ray Diffraction (XRD) Analysis

The OPEFB, PLA, MWCNTs, and OPEFB/PLA/MWCNTs composites were characterized to study the effect of MWCNTs on the OPEFB/PLA composites' crystallinity. As presented in Figure 4, the XRD patterns of pure PLA showed a wide diffraction peak of approximately  $2\theta \approx 18^\circ$ . The PLA showed no characteristic peak and indicated that PLA has an amorphous structure (Challabi *et al.*, 2019). The OPEFB also exhibits peaks at  $2\theta \approx 16^\circ$  and  $2\theta \approx 24^\circ$ , indicating amorphous and crystalline regions (Harun *et al.*, 2013). Cellulosic natural fibers contain both crystalline (ordered) and amorphous (disordered). Thus, the existence of dual features in the fiber is consistent with the presence of ordered and disordered regions (Ali *et al.*, 2015). The broad peaks of OPEFB suggest a carbon-based and cellulose-type material (Abdalhadi *et al.*, 2018).

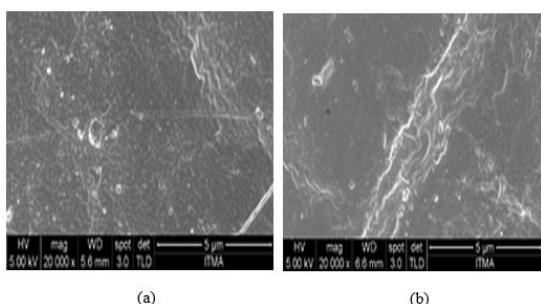
The MWCNTs XRD pattern displays a wide diffraction peak at  $2\theta \approx 26.2^\circ$  that corresponds to (002) and a small peak at  $2\theta \approx 44.2^\circ$  corresponding to (100), indicating the crystalline structure of MWCNTs (Bibi *et al.*, 2017). Moreover, the OPEFB/MWCNTs nanocomposites showed characteristic diffraction peaks at  $2\theta \approx 26.2^\circ$  and  $2\theta \approx 44.2^\circ$ . The high diffraction peak at  $26.2^\circ$  may be due to the MWCNTs stacking layers with the disorder (002) (Ahmad *et al.*, 2025).



**Figure 4.** XRD pattern of OPEFB, PLA, MWCNTs, and OPEFB/PLA/MWCNTs composites with different concentrations of MWCNTs.

#### Field emission scanning electron microscopy (FE-SEM) Analysis

The FE-SEM images in Figure 4a, b showed the morphology of OPEFB/PLA/5wt. % MWCNTs and OPEFB/PLA/13wt. % MWCNTs nanocomposites. The MWCNTs bind strongly to the OPEFB/PLA matrix surface and tips due to the effectiveness of the Brabender mixer as can be seen in the FESEM images. The uniform dispersion of the hybrid filler particles in polymer systems leads to the creation of a co-supportive network that is likely to strengthen composite electrical conductivity. Nanocomposite's network structure with a high available surface area is expected to contribute to various interfacial polarization resulting in the weakening of the EM waves (Ravindren *et al.*, 2019).

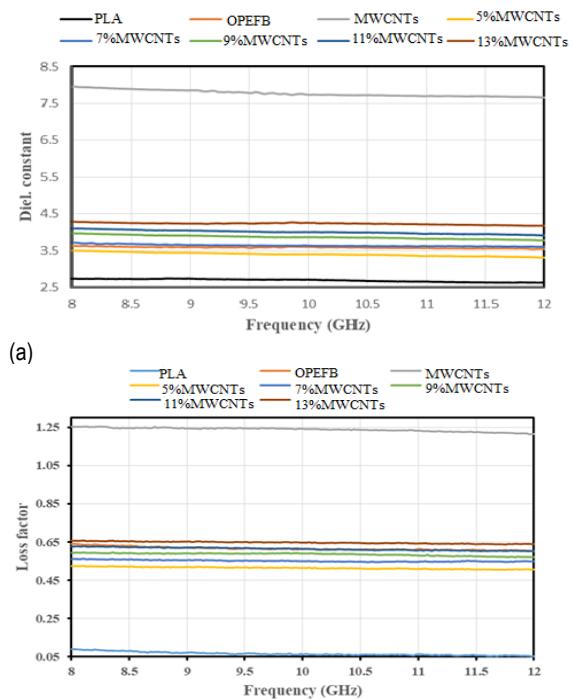


**Figure 4.** FE-SEM images of (a) OPEFB/PLA/5% MWCNTs (b) OPEFB/PLA/13% MWCNTs

#### Dielectric Properties Analysis

Figure 5 displays the complex permittivity of the OPEFB fibers and MWCNTs and the frequency variation. Generally, dielectric constant ( $\epsilon'$ ) and loss factor ( $\epsilon''$ ) values of both OPEFB fiber and MWCNTs decreased with frequency increase, as described by the Maxwell-Wenger polarization model (Maleknejad *et al.*, 2016). The MWCNTs had higher  $\epsilon'$  and  $\epsilon''$  values in the 8-12 GHz range than the OPEFB fiber. The OPEFB fiber and MWCNTs  $\epsilon'$  values were

3.57 and 7.65, while the  $\epsilon''$  values were 0.63 and 1.24, respectively.



**Figure 5.** variation in: (a) dielectric constant and (b) loss factor of OPEFB/PLA/MWCNTs

The effect of the 5-13 wt.% MWCNTs filler on the dielectric of OPEFB/PLA/MWCNTs composites was studied, and the variation in  $\epsilon'$  and  $\epsilon''$  values in the range 8-12 GHz is shown in Figure 5. It has been reported that the quality of conductive fillers distributed in a polymer matrix will play a significant role in the entire sample's dielectric behaviors (Mensah *et al.*, 2019). PLA has low permittivity because the small amount of macromolecular polarization. The values of  $\epsilon'$  and  $\epsilon''$  in the 8-12 GHz range decreased with frequency for the 5-13 wt.% composites. The complex permittivity values for the composites depend primarily on the contribution of interfacial, orientation, and electronic and atomic polarization in the material, due to the differences in the polarization or conductivity of the matrix and the filler. The results show that the complex permittivity of OPEFB/PLA composites can be increased significantly by the addition of MWCNTs.

#### Material Reflectance and Absorbance Loss

The S-parameters ( $S_{11}$  and  $S_{21}$ ) can be conveniently correlated with reflectance ( $R$ ) and transmittance ( $T$ ), where,

$$T = \left| \frac{E_T}{E_I} \right|^2 = |S_{21}|^2 \quad (3.1)$$

$$R = \left| \frac{E_R}{E_I} \right|^2 = |S_{11}|^2 \quad (3.2)$$

Giving absorbance ( $A$ ) as,

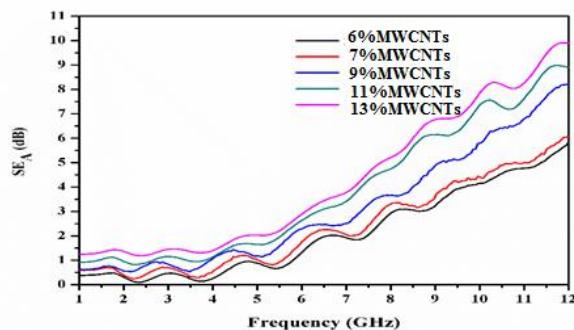
$$A = (1 - T - R) \quad (3.3)$$

$$A = (1 - |S_{21}|^2 - |S_{11}|^2) \quad (3.4)$$

$SE_A$  can be determined by the following equations;

$$SE_A = -10 \log_{10} \left( \frac{T}{1-R} \right) \quad (3.5)$$

The microstrip is a free-space technique where waves can radiate at the input and output as well as along the sample. The variation of the absorption ( $SE_A$ ) component of the EMI shielding against the frequency for the OPEFB-PLA-MWCNTs composites is shown in Figure 6. The  $SE_A$  values of the composites increased across the 8-12 GHz. The increment ranges from 3.06 at 8 GHz to 9.91 dB at 11.85 GHz. There is no substantial variation in the values of  $SE_A$ , considering 5 to 13 wt.% composites. This small variation is probably due to measurement uncertainties during the permittivity measurements. These findings demonstrate that the OPEFB-PLA-MWCNTs are capable of significant microwave absorption and should act as a cheaper and more effective option for applications throughout the investigated frequency range.



**Figure 6.** Variation in absorption loss ( $SE_A$ ) for the OPEFB-PLA-MWCNTs nano composites

### Conclusion

The composite material consisting of OPEFB fiber, PLA, and MWCNTs was successfully synthesized via the melt-blend technique. XRD analysis reveals that the increasing addition of MWCNTs in the composite will result in the increase in slight increase in the relative intensity due to the MWCNTs stacking layers with the disorder (002). FESEM micrographs show that the MWCNTs bind well with the OPEFB/PLA matrix. Electromagnetic measurement reveals promising values of EMI shielding effectiveness through absorption. The increase in MWCNTs results in the enhanced performance of the shielding effectiveness.

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